

NASA Vision & Mission

NASA vision is:

- Innovation
- Exploration
- Discovery

The NASA mission is:

- Technology innovation
- Inspiration for the next generation
- And discovery in our universe as only NASA can



Limits to Open Class Performance?



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Annual Convention of the

Soaring Society of America

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Dedicated to the memory of Dr Paul MacCready

It seems that perfection is attained
Not when there is no more to be added,
But when there is nothing more to be deleted.
At the end of its evolution,
The machine effaces itself.

- Antoine de Saint-Exupery



Intro

- Standard Class
- 15m/Racing Class
- Open Class
- Design Solutions
 - assumptions
 - limiting parameters
 - airfoil performance
 - current trends
 - analysis
- Conclusions

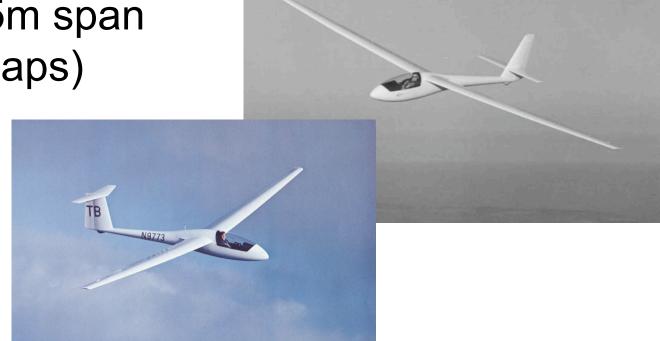


Standard Class

Q: What is the size limitation in the

Standard Class?

 A: 15m span (no flaps)



15m/Racing Class

- Q: What is the 15m size limitation?
- A: 15m span (no restriction on flaps)





Open or Unlimited Class

Q: What is the size limitation on the

Open Class?





Open Class Limitation: MASS!

• 650 kg single-place

750 kg two-place

 850 kg two-place w/ motor





- Assumptions:
 - no active boundary layer control
 - use current technology materials fiberglass carbon fiber
 - fits within existing rules
 - no variable geometry (camber changing flaps only)
 - no active controls (no unstable designs)

Limiting Parameters

- Reynolds number
 - chord limitations: viscous drag
 - max CL
- Mass increases faster than span modern materials help
- Still need to fly slow, turn and bank
- Still need to dash fast

Limiting Parameters

- Slow climbing flight requires low wing loading
- High cruise speed requires high wing loading
- Minimum sink requires low speed
- Max L/D balances viscous and induced drag
- Low viscous drag is always desirable
- The 'best" sailplane will always be versatile
- Note: gains in either induced or viscous drag alone will net only half the gain overall!
- Note: other structural problems (yaw inertia & spins, flutter, static loads integrity)

Airfoil Limitations

- Thickness constraints
- Flaps allow thinner (and lower Cdo) airfoils (with limitations)
- Laminar flow drag bucket is roughly in proportion to thickness (NB: Std Class t/c ~17%; 15m/Open Class t/c ~14%)
- Approximately 60% to 75% of total viscous drag of Open Class designs is airfoil profile drag

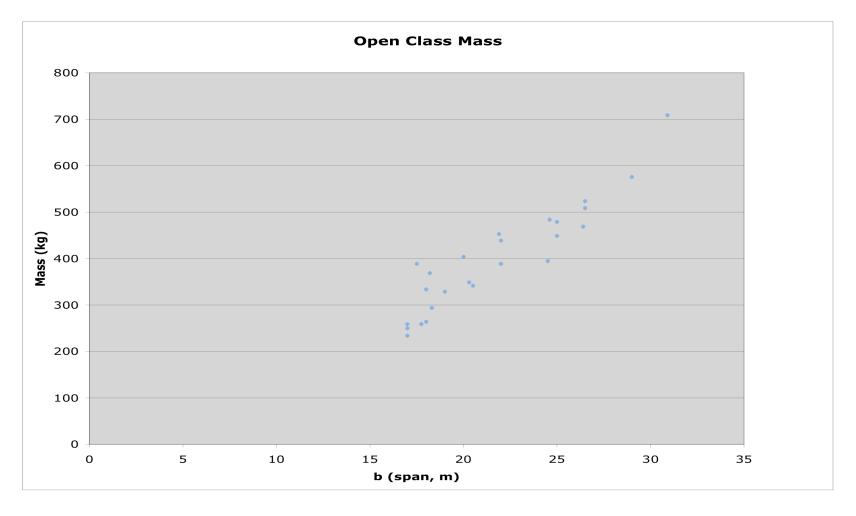
Current Trends

Survey of the Open Class (composites)

company	model	span	L/D	We
Glasflugel	BS-1	18	44	335
	Kestrel 17	17	43	260
	604	22	49	440
Schempp-Hirth	Cirrus	17.74	44	260
	Nimbus II	20.3	49	350
	Ventus 2C	18	46	265
	Nimbus 3	24.5	58	396
	Nimbus 4	26.4	60	470
Schleicher	AS-W12	18.3	47	295
	AS-W 17	20	48.5	405
	AS-W 22	25	60	450
Akaflieg Braunschweig	SB-10	29	53	577
PZL	Jantar 2	20.5	47	343
MBB	Pheobus C	17	42	235
Slingsby	Kestrel 19	19	44	330
	Kestrel 22	22	51.5	390
Glasar Dirks	DG-202	17	45	251
Applebay	Mescalero	21.9	44	454
Grob	G-103 Twin Astir	17.5	38	390
Schempp-Hirth	Janus	18.2	39	370
	Nimbus 3D	24.6	57	485
	Nimbus 4D	26.5	60	525
Schleicher	AS-H 25	25	57	480
	AS-H 30	26.5	61.8	510
Eta	Eta	30.9	70	710

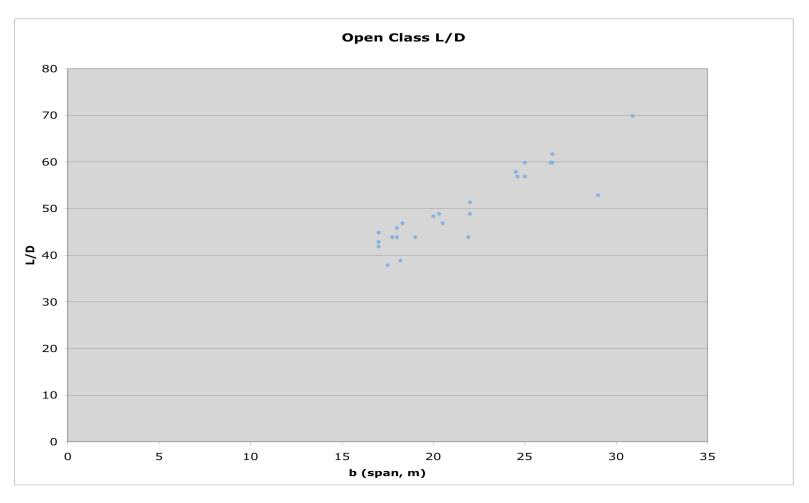
Current Trends (Mass)

Open Class mass (kg)



Current Trends (L/D)

Open Class (L/D)

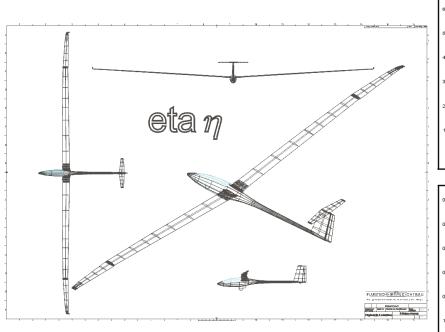


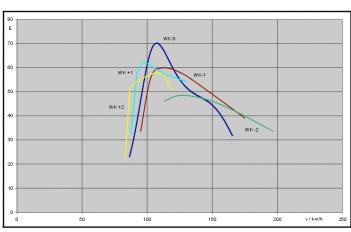
Analysis

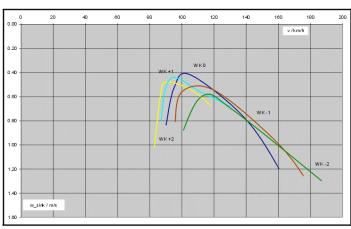
- Eta is the current performance benchmark
- Near elliptical span load
- 30.9m span
- 710 kg empty
- 70:1 L/D
- Yaw inertia



Eta







Spanload Development

Ludwig Prandtl

Development of the boundary layer concept (1903)

Developed the "lifting line" theory

Developed the concept of induced drag

Calculated the spanload for minimum induced drag (1908?)

Published in open literature (1920)

Albert Betz

Published calculation of induced drag

Published optimum spanload for minimum induced drag (1914)

Credited all to Prandtl (circa 1908)

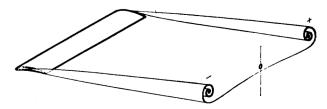
Spanload Development (continued)

- Max Munk
 General solution to multiple airfoils
 Referred to as the "stagger biplane theorem" (1920)
 Munk worked for NACA Langley from 1920 through 1926
- Prandtl (again!)
 "The Minimum Induced Drag of Wings" (1932)
 Introduction of new constraint to spanload
 Considers the bending moment as well as the lift and induced drag

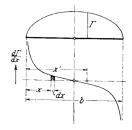
Practical Spanload Developments

- Reimar Horten (1945)
 Use of Prandtl's latest spanload work in sailplanes & aircraft Discovery of induced thrust at wingtips Discovery of flight mechanics implications Use of the term "bell shaped" spanload
- Robert T Jones
 Spanload for minimum induced drag and wing root bending moment
 Application of wing root bending moment is less general than Prandtl's
 No prior knowledge of Prandtl's work, entirely independent (1950)
- Armin Klein & Sathy Viswanathan
 Minimum induced drag for given structural weight (1975)
 Includes bending moment
 Includes shear

Prandtl Lifting Line Theory

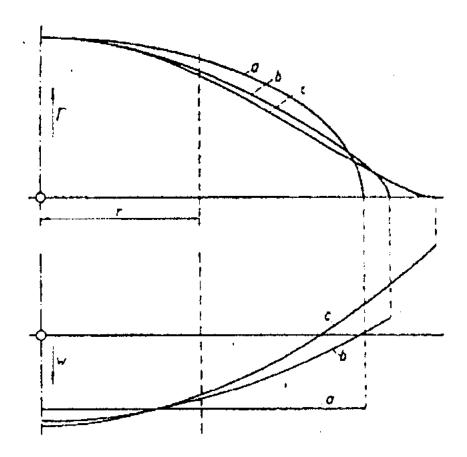


Prandtl's "vortex ribbons"



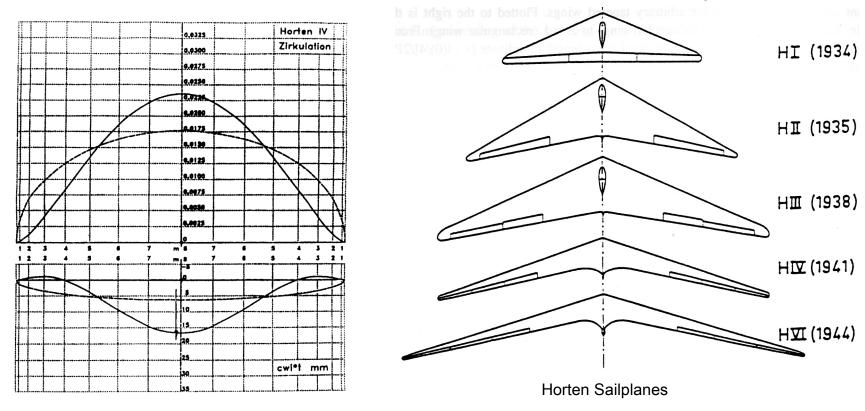
- Elliptical spanload (1914)
- "the downwash produced by the longitudinal vortices must be uniform at all points on the aerofoils in order that there may be a minimum of drag for a given total lift." y = c

Minimum Induced Drag & Bending Moment



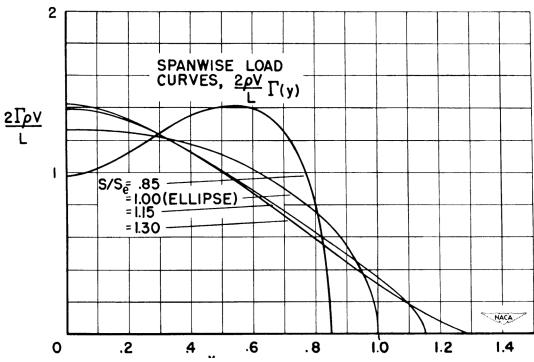
Prandtl (1932)
 Constrain minimum induced drag
 Constrain bending moment
 22% increase in span with 11% decrease in induced drag

Horten Applies Prandtl's Theory



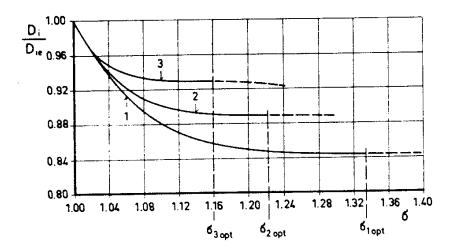
 Horten Spanload (1940-1955) induced thrust at tips wing root bending moment

Jones Spanload



- Minimize induced drag (1950)
 Constrain wing root bending moment
 30% increase in span with 17% decrease in induced drag
- "Hence, for a minimum induced drag with a given total lift and a given bending moment the downwash must show a linear variation along the span." y = bx + c

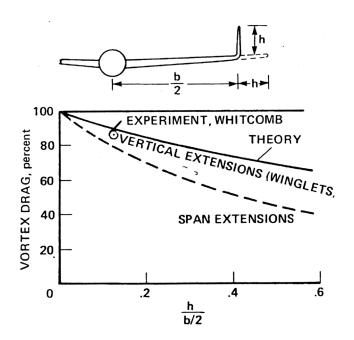
Klein and Viswanathan

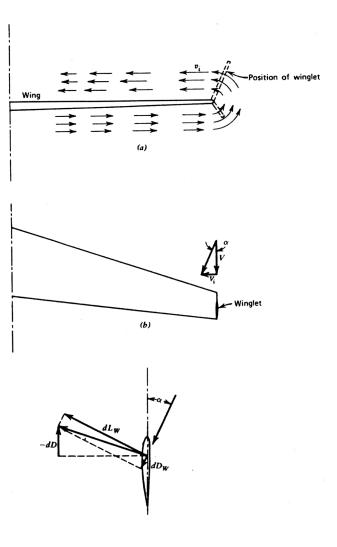


- Minimize induced drag (1975)
 Constrain bending moment
 Constrain shear stress
 16% increase in span with 7% decrease in induced drag
- "Hence the required downwash-distribution is parabolic." y = ax + bx + c

Winglets

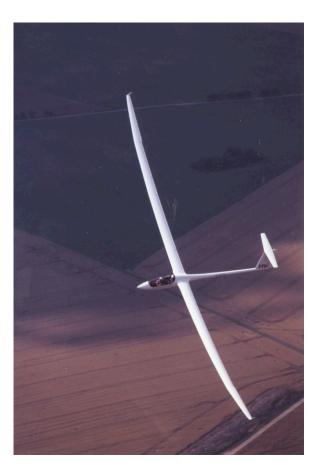
- Richard Whitcomb's Winglets
 - induced thrust on wingtips
 - induced drag decrease is about half of the span "extension"
 - reduced wing root bending stress





- Minimum induced drag for a given span: elliptical span load (or winglets)
- Minimum induced drag for a given structural weight: bell shaped span load (16% greater span and 7% less drag than elliptical - Klein & Viswanathan)

- Applying bell shaped span load to Eta-class sailplane
- 710 kg We (plus two 70 kg pilots)
- 7% less induced drag
- 16% more span (36m!)
- Max L/D = \sim 72:1

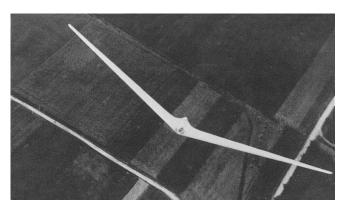


- What if we could build a flying wing?
- Decrease viscous drag by 15% (can't take full credit for 25%)
- Decrease induced drag by 7%



Flying Wing

- Balance between induced and viscous drag gives about 12% total drag decrease
- Optimistic due to additional constraint of pitching moment from wing
- Max L/D = 78:1
- Even if the airfoil Cdo was 40% of the total, & all credit was taken: Max L/D ~ 94:1



Horten H VI

Conclusions

- Open Class performance limits (under current rules and technologies) is very close to absolute limits
- Some gains remain to be explored
- Possible gains from unexplored areas and new technologies, even using existing materials.



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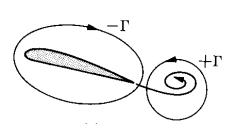
What does the future hold?

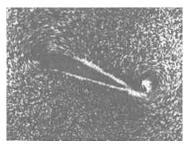


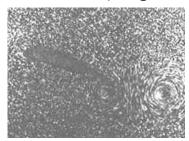
Start-Up Vortex



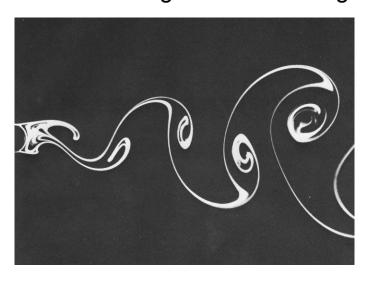
Prandtl's lifting-line theory - conservation of momentum (angular)

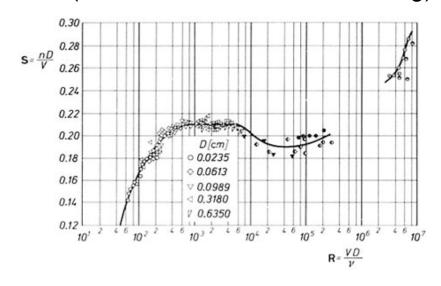






• Oscillating vortex shedding - Strouhal (nondimensional vortex shedding)





And what are we still missing?



Thanks to Phil Barnes and Bob Hoey for reminding us...